

The Relative Velocity between Two Confocal Keplerian Orbits

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Abstract

We derive analytically the relative velocity vector and relative velocity magnitude between two particles on confocal Keplerian orbits.

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1 Introduction

Hilton et al. 1996 [1] and Hilton 2002 [2] used a two-body scattering angle as a filter for determining significant asteroid-asteroid close approaches. The scattering angle φ in the center-of-mass frame is given by

$$\tan \frac{\varphi}{2} = \frac{G(m_1 + m_2)}{v^2 b} \quad (1)$$

where m_1 and m_2 are the asteroid masses, b is the impact parameter, and v is the magnitude of the relative encounter velocity. Thus, the relative encounter speed is important to the observed effects of an encounter deflection. It is possible for a distant encounter at low relative speed to suffer a larger deflection than a closer encounter at higher relative speed. In this Note, we calculate explicitly the relative encounter velocity and its magnitude for two confocal Keplerian orbits, in terms of relative orbital elements $\{\alpha, e_1, e_2, \iota, \omega, \Omega; E_1, E_2\}$. First, however, we present the relative elements in terms of the orbital elements of the two orbits with respect to some inertial frame, $\{a_k, e_k, \iota_k, \omega_k, \Omega_k, M_k\}$, $k = 1, 2$.

2 Relative Elements and the Relative Distance Vector

Consider the set of relative orbital elements $\{\alpha, e_1, e_2, \iota, \omega, \Omega; E_1, E_2\}$, where

$$\alpha = \frac{a_2}{a_1}, \quad (2)$$

the relative orientation elements $\{\iota, \omega, \Omega\}$ are as shown in Figure 1, and $E_1(t)$ and $E_2(t)$ are the eccentric anomalies of the two bodies. The transformation from separate orbital elements for each orbit to relative elements is given by (Murison and Munteanu 2007 [3])

$$\left. \begin{aligned} \cos\Omega \sin\iota &= \sin\omega_1 \sin\iota_2 \sin\Delta\Omega - \cos\omega_1 (\sin\iota_1 \cos\iota_2 - \cos\iota_1 \sin\iota_2 \cos\Delta\Omega) \\ \sin\Omega \sin\iota &= \cos\omega_1 \sin\iota_2 \sin\Delta\Omega + \sin\omega_1 (\sin\iota_1 \cos\iota_2 - \cos\iota_1 \sin\iota_2 \cos\Delta\Omega) \\ \cos\omega \sin\iota &= \sin\omega_2 \sin\iota_1 \sin\Delta\Omega + \cos\omega_2 (\cos\iota_1 \sin\iota_2 - \sin\iota_1 \cos\iota_2 \cos\Delta\Omega) \\ \sin\omega \sin\iota &= -\cos\omega_2 \sin\iota_1 \sin\Delta\Omega + \sin\omega_2 (\cos\iota_1 \sin\iota_2 - \sin\iota_1 \cos\iota_2 \cos\Delta\Omega) \\ \cos\iota &= \cos\iota_1 \cos\iota_2 + \sin\iota_1 \sin\iota_2 \cos\Delta\Omega \end{aligned} \right\} \quad (3)$$

where $\Delta\Omega = \Omega_2 - \Omega_1$. The eccentric anomalies can be calculated from the respective mean anomalies via the Kepler equation,

$$E(t) - e \sin E(t) = M(t) = n(t - \tau) = M_0 + n(t - t_0) \quad (4)$$

where M_0 is the mean anomaly at epoch $t = t_0$, τ is a time of pericenter passage, and n is the mean motion $2\pi/T$ with T the orbital period. With equations (3) and (4) we may transform from separate orbital elements with respect to some inertial frame at epoch t_0 to relative elements.

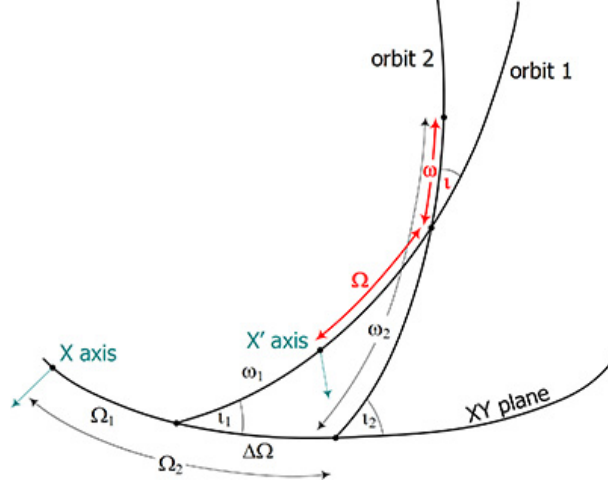


Figure 1: Relative orbital elements.

In terms of the relative elements, and with respect to a coordinate frame whose x axis is along the pericenter and z axis is parallel to the angular momentum vector of orbit 1, the relative distance vector is

$$\frac{1}{a_1} \vec{R}(t) = \frac{1}{a_1} (\vec{r}_2 - \vec{r}_1) = \alpha \mathcal{Q}(\Omega, \iota, \omega) \cdot \vec{q}(E_2) - \vec{q}(E_1) \quad (5)$$

where in general a Keplerian orbit may be expressed in the form $\vec{r} = a\mathcal{Q}(\Omega, \iota, \omega) \cdot \vec{q}(E)$, where the vector

$$\vec{q}(E) = \begin{bmatrix} \cos E - e \\ \sqrt{1 - e^2} \sin E \\ 0 \end{bmatrix} \quad (6)$$

specifies the position along the orbit path, and the orbit orientation matrix $\mathcal{Q}(\Omega, \iota, \omega)$ is a product of three orthogonal rotations,

$$\mathcal{Q}(\Omega, \iota, \omega) = \begin{bmatrix} \cos\Omega \cos\omega - \sin\Omega \sin\omega \cos\iota & -\cos\Omega \sin\omega - \sin\Omega \cos\omega \cos\iota & \sin\Omega \sin\iota \\ \sin\Omega \cos\omega + \cos\Omega \sin\omega \cos\iota & -\sin\Omega \sin\omega + \cos\Omega \cos\omega \cos\iota & -\cos\Omega \sin\iota \\ \sin\omega \sin\iota & \cos\omega \sin\iota & \cos\iota \end{bmatrix} \quad (7)$$

This formulation cleanly separates the orbit scale a , the shape of the orbit e plus the position of the particle at a given time \vec{q} , and the orientation of the orbit in space $\mathcal{Q}(\Omega, \iota, \omega)$.

3 Relative Velocity

Differentiation of the relative distance vector yields the relative velocity vector,

$$\frac{1}{a_1} \vec{V}(t) = \frac{1}{a_1} \frac{d\vec{R}}{dt} = \alpha \mathcal{Q}(\Omega, \iota, \omega) \cdot \frac{d\vec{q}(E_2(t))}{dt} - \frac{d\vec{q}(E_1(t))}{dt} \quad (8)$$

Now, from the Kepler equation (4), we have

$$\dot{E} = \frac{n}{1 - e \cos E} \quad (9)$$

Define a mass parameter

$$\mu_k \equiv G(M + m_k), \quad k \in \{1, 2\} \quad (10)$$

where M is the central mass. Since $M \gg m_k$,

$$\frac{\mu_2}{\mu_1} = \frac{M + m_2}{M + m_1} = \frac{1 + \varepsilon_2}{1 + \varepsilon_1} = 1 + \varepsilon_2 - \varepsilon_1 - \varepsilon_1 \varepsilon_2 + \varepsilon_1^2 - \dots \quad (11)$$

where $\varepsilon_k = \frac{m_k}{M}$. Thus, for the asteroids $\frac{\mu_2}{\mu_1} \approx 1$ and $\mu_1 \approx \mu_2 \approx GM_\odot \equiv \mu_\odot$. The mean motion and semimajor axis are related by Kepler's third law, $\mu = n^2 a^3$ (where, in general, μ is G times the sum of the two masses). Hence, we may generally write

$$\frac{d\vec{q}}{dt} = \frac{\partial \vec{q}}{\partial E} \dot{E} = \frac{n}{1 - e \cos E} \frac{\partial \vec{q}}{\partial E} = \frac{1}{1 - e \cos E} \sqrt{\frac{\mu}{a^3}} \begin{bmatrix} -\sin E \\ \sqrt{1 - e^2} \cos E \\ 0 \end{bmatrix} \quad (12)$$

Let $\beta = \alpha - 1 = \frac{a_2 - a_1}{a_1}$. Then the relative velocity, (8), becomes

$$\sqrt{\frac{a_1}{\mu_\odot}} \vec{V}(t) = \sqrt{\frac{1}{1 + \beta}} \frac{1}{1 - e_2 \cos E_2} \mathcal{Q}(\Omega, \iota, \omega) \cdot \frac{\partial \vec{q}(E_2)}{\partial E_2} - \frac{1}{1 - e_1 \cos E_1} \frac{\partial \vec{q}(E_1)}{\partial E_1} \quad (13)$$

where the velocity is scaled by the velocity of a circular orbit of radius a_1 ,

$$n_1 a_1 = \sqrt{\frac{\mu_\odot}{a_1}} \quad (14)$$

In component form, eq. (13) is

$$\begin{aligned} \sqrt{\frac{a_1}{\mu_\odot}} \vec{V}(t) &= \frac{1}{1 - e_2 \cos E_2} \frac{\vec{B}(E_1, E_2)}{\sqrt{1 + \beta}} - \frac{1}{1 - e_1 \cos E_1} \begin{bmatrix} -\sin E_1 \\ \sqrt{1 - e_1^2} \cos E_1 \\ 0 \end{bmatrix} \\ &= \frac{1 - \frac{1}{2}\beta + \frac{3}{8}\beta^2 - \dots}{1 - e_2 \cos E_2} \vec{B}(E_1, E_2) - \frac{1}{1 - e_1 \cos E_1} \begin{bmatrix} -\sin E_1 \\ \sqrt{1 - e_1^2} \cos E_1 \\ 0 \end{bmatrix} \end{aligned} \quad (15)$$

where

$$\vec{B}(E_1, E_2) = \begin{bmatrix} C_2\sqrt{1-e_2^2}\cos E_2 - C_4\sin E_2 \\ C_1\sqrt{1-e_2^2}\cos E_2 - C_3\sin E_2 \\ (\cos\omega\sqrt{1-e_2^2}\cos E_2 - \sin\omega\sin E_2)\sin\iota \end{bmatrix} \quad (16)$$

and

$$\left. \begin{aligned} C_1 &= -\sin\Omega \sin\omega + \cos\Omega \cos\omega \cos\iota \\ C_2 &= -\cos\Omega \sin\omega - \sin\Omega \cos\omega \cos\iota \\ C_3 &= \sin\Omega \cos\omega + \cos\Omega \sin\omega \cos\iota \\ C_4 &= \cos\Omega \cos\omega - \sin\Omega \sin\omega \cos\iota \end{aligned} \right\} \quad (17)$$

Upon squaring (15), we find the relative velocity magnitude,

$$\frac{a_1}{\mu_\odot} \left\| \vec{V}(t) \right\|^2 = \frac{1+e_1\cos E_1}{1-e_1\cos E_1} + \frac{1}{1+\beta} \frac{1+e_2\cos E_2}{1-e_2\cos E_2} - \frac{2}{\sqrt{1+\beta}} \frac{g(E_1, E_2)}{(1-e_1\cos E_1)(1-e_2\cos E_2)} \quad (18)$$

where

$$\begin{aligned} g(E_1, E_2) &= \sqrt{1-e_2^2}\cos E_2 \left(C_1\sqrt{1-e_1^2}\cos E_1 - C_2\sin E_1 \right) \\ &\quad - \sin E_2 \left(C_3\sqrt{1-e_1^2}\cos E_1 - C_4\sin E_1 \right) \end{aligned} \quad (19)$$

An optimized C function to calculate eq. (18) is shown in the Appendix (Section 4). For completeness, expanding on ε , we have

$$\begin{aligned} \frac{a_1}{\mu_\odot} \left\| \vec{V}(t) \right\|^2 &= \frac{1+e_1\cos E_1}{1-e_1\cos E_1} + \frac{1+e_2\cos E_2}{1-e_2\cos E_2} (1 - \beta + \beta^2 - \dots) \\ &\quad - \frac{2g(E_1, E_2)}{(1-e_1\cos E_1)(1-e_2\cos E_2)} \left(1 - \frac{1}{2}\beta + \frac{3}{8}\beta^2 - \dots \right) \end{aligned} \quad (20)$$

References

- [1] Hilton, J.L., Seidelmann, P.K., and Middour, J. (1996), “Prospects for Determining Asteroid Masses”, *Astronomical Journal* **112**, 2319-2329.
- [2] Hilton, J.L. (2002), “Asteroid Masses and Densities”, in *Asteroids III*, eds. Bottke et al., University of Arizona Press, Tuscon, pp. 103-112.
- [3] Murison, M.A., and Munteanu, A. (2007), “On the Distance Function between Two Confocal Keplerian Orbits”, submitted to *Astronomical Journal*.

4 Appendix: Optimized C Code for the Squared Relative Velocity

```
double vsquared( double E1, double E2, double e1, double e2,
                 double beta, double iota, double peri, double node )
{
    double t6 = sin(node);
    double t7 = cos(peri);
    double t19 = t6*t7;
    double t5 = cos(node);
    double t18 = t5*t7;
    double t8 = sin(peri);
    double t17 = t6*t8;
    double t16 = t5*t8;
    double t11 = cos(E2);
    double t1 = e2*e2;
    double t20 = sqrt(1.0-t1);
    double t15 = t20*t11;
    double t14 = e2*t11;
    double t12 = cos(E1);
    double t13 = e1*t12;
    double t10 = sin(E2);
    double t9 = cos(iota);
    double t4 = 1.0+beta;
    double t2 = 1.0/(t13-1.0);
    double t24 = sqrt(t4);
    double t34 = e1*e1;
    double t36 = sqrt(1.0-t34);
    double t45 = sin(E1);
    return ( (-t13-1.0)*t2
            + ( -2.0/t24*( t12*((-t17+t9*t18)*t15-(t19+t9*t16)*t10)*t36
                    + ((t9*t19+t16)*t15-(t18+t9*t17)*t10)*t45 )*t2
            + (-t14-1.0)/t4 )/(-1.0+t14) );
}
```